



ADDENDUM NO. 2
TO THE CONTRACT DOCUMENTS

Date: September 18, 2018
CH2M HILL Project No.: 691267

for the
Brooks Bridge Water Main Replacement for the Okaloosa Island Water Supply Project

To All Plan Holders:

The following changes, additions, and/or deletions are hereby made part of the Contract Documents for the Brooks Bridge Water Main Replacement Project, dated August 2018, as fully and completely as if the same set forth fully therein:

Specifications

A. OCWS Contractor Procurement Front End

SECTION C-451, Qualifications Statement

1. Page 6, REPLACE in its entirety with the attached revised page 6 of the Qualifications Statement.

SECTION C-520, Agreement

2. Page 2, Section 4.02 CHANGE "...within 45 days after the date when the Contract Times commence to run." TO "...within 225 days after the date when the Contract Time commence to run."

B. TECHNICAL SPECIFICATIONS

SECTION 01 29 00, Payment Procedures

1. Page 2, Section 1.05 A CHANGE "No partial payments based upon percentage of completion or stored materials will be awarded." TO "If requested by the Contractor, partial payments will be awarded for mobilization. Contractor to submit invoices for bonds and insurance certificates with pay application. No partial payments based upon percentage of completion or stored materials will be awarded for the 20-in Diameter HDPE Directional Drill and Erosion Control Measures line items as shown on the Bid Sheet."

SECTION 01 50 00, Temporary Facilities and Controls

1. Page 3, Section 3.01 C.1 CHANGE "Hydrant Water" TO "Hydrant Water: Okaloosa Island"
2. Page 3, ADD Section 3.01 C.2 and C.3
"2. Hydrant Water: Ft. Walton Beach

- a. Hydrant water is available for construction purposes for all activities located on the Ft. Walton Beach side of the project from the City of Ft. Walton Beach, FL.
- b. Contractor to submit a meter order form to the City of Ft. Walton Beach prior to beginning construction and will be responsible for all costs associated with utilizing water from the City.

3. Water Processing and Disposal

- a. Contractor is responsible for obtaining, handling and disposal of all water used onsite for all construction activities including pipe flushing and pressure testing. Contractor shall obtain any required permits and shall be responsible for adhering to all local, state, and federal rules that pertain to the disposal of the water.”

3. Page 7, Section 3.03 B CHANGE “Noise Ordinance Control: City of Ft. Walton Beach” TO “Noise Ordinance Control: City of Ft. Walton Beach and Okaloosa County, FL”

4. Page 10, CHANGE Section 3.08 to Section 3.09 and ADD Section 3.08:

“SITE RESTORATION

- a. All disturbed areas of the project site shall be returned to their preconstruction conditions, including, but not limited to, driveways and grassed areas. If disturbed during construction the property bordering the Okaloosa Island Fire Station shall be returned to preconstruction site conditions including replacing existing sod with the same sod type and condition; as well as irrigation systems, etc.
- b. OCWS will be responsible for the removal and replacement of fencing and retaining walls within the County-owned property boundaries on the Okaloosa Island portion of the project. Contractor to inform the OCWS the extent of fencing that needs removal prior to construction. “

SECTION 33 05 01, High-Density Polyethylene (HDPE) Pressure Pipe and Fittings

1. Page 9, Section 3.03 ADD the following paragraph: “C. Disinfection of new pipe to be performed by OCWS.”

SECTION 33 05 23, Utility Horizontal Directional Drilling

- 1. Page 3, Section 3.04 D CHANGE “A single stage pull should be performed but no more than a 2-stage pull or one intermediate weld will be permitted while pulling pipe.” TO “Contractor shall limit the number of individual pullbacks based on available area for pipe string staging, but no more than 4 pullbacks, or the number that the Contractor deems technically feasible without compromising the pullback, whichever is less.”
- 2. Page 3, Section 3.04 E DELETE “Staging of pipe on the Okaloosa Island side, as shown on the drawings, is an available option.”

3. Page 4, Section 3.11: DELETE Supplement A.2 and REPLACE with the attached HDD Report.

B. PART 4 - DRAWINGS

1. DELETE drawing sheets C-01, C-02, C-03, and C-04 and REPLACE with the drawings attached.

Questions Received during Advertisement for Bid Period

1. What is the project budget?
 - a. The construction estimate is \$460,000.

Attachments

1. Qualifications Statement
2. Revised Contract Drawings C-01, C-02, C-03, and C-04
3. Mandatory Pre-Bid Meeting Minutes
4. CH2M HDD Report dated June 2017

All Bidders shall acknowledge receipt of this Addendum.

Name of Contractor's Safety Officer: _____

Include the following as attachments:

Provide as an Attachment Contractor's (and Contractor's proposed Subcontractors and Suppliers furnishing or performing Work having a value in excess of 10 percent of the total amount of the Bid) OSHA No. 300- Log & Summary of Occupational Injuries & Illnesses for the past 5 years.

Provide as an Attachment Contractor's (and Contractor's proposed Subcontractors and Suppliers furnishing or performing Work having a value in excess of 10 percent of the total amount of the Bid) list of all OSHA Citations & Notifications of Penalty (monetary or other) received within the last 5 years (indicate disposition as applicable) - IF NONE SO STATE.

Provide as an Attachment Contractor's (and Contractor's proposed Subcontractors and Suppliers furnishing or performing Work having a value in excess of 10 percent of the total amount of the Bid) list of all safety citations or violations under any state all received within the last 5 years (indicate disposition as applicable) - IF NONE SO STATE.

Provide the following for the firm listed in Section V (and for each proposed Subcontractor furnishing or performing Work having a value in excess of 10 percent of the total amount of the Bid) the following (attach additional sheets as necessary):

Workers' compensation Experience Modification Rate (EMR) for the last 5 years:

YEAR	_____	EMR	_____
YEAR	_____	EMR	_____
YEAR	_____	EMR	_____
YEAR	_____	EMR	_____
YEAR	_____	EMR	_____

Total Recordable Frequency Rate (TRFR) for the last 5 years:

YEAR	_____	TRFR	_____
YEAR	_____	TRFR	_____
YEAR	_____	TRFR	_____
YEAR	_____	TRFR	_____
YEAR	_____	TRFR	_____

13. EQUIPMENT:

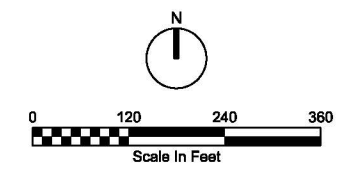
MAJOR EQUIPMENT:

List on **Schedule C** all pieces of major equipment available for use on Owner's Project.

- NOTES:**
- FUSED PIPE STAGING ALIGNMENT OPTION IS SHOWN. CONTRACTOR TO SUBMIT PROPOSED STAGING PLAN ALONG WITH TRAFFIC CONTROL PLAN. CONTRACTOR TO PROVIDE TRAFFIC CONTROL AND TEMPORARY ACCESS WHILE STAGING FOR FUSED PIPE. PROVIDE MEANS OF INGRESS AND EGRESS TO ALL RESIDENCES AND BUSINESSES DURING CONSTRUCTION.
 - SEE SHEET C-03 AND C-04 FOR LIMITS OF WORK AND CONTRACTOR RESPONSIBILITY.
 - SEE GENERAL CONSTRUCTION NOTES ON SHEET G-02.

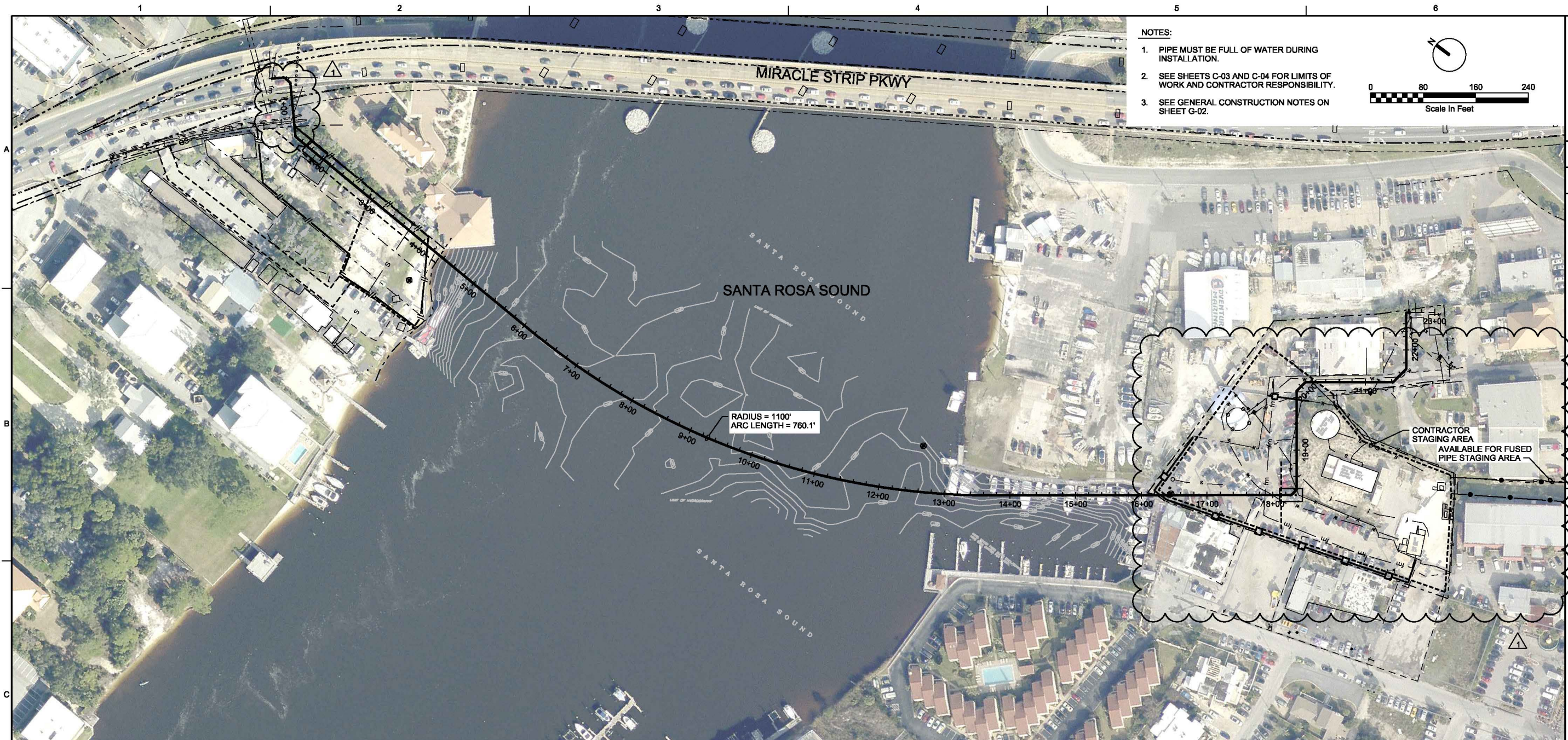
CONTROL POINTS

- RSM CONTROL POINT #104158
 NAIL & DISC LS #5791 (SET)
 NORTHING: 514938.5940'
 EASTING: 1306262.4610'
 ELEVATION: 2.91'
- RSM CONTROL POINT #104160
 CAPPED IRON ROD LS #5791 (SET)
 NORTHING: 515006.2630'
 EASTING: 1306251.6790'
 ELEVATION: 3.27'
- RSM CONTROL POINT #104156
 CAPPED IRON ROD LS #5791 (SET)
 NORTHING: 514939.1590'
 EASTING: 1306118.4560'
 ELEVATION: 3.13'
- RSM CONTROL POINT #104213
 CAPPED IRON ROD LS #5791 (SET)
 NORTHING: 515825.0280'
 EASTING: 1305877.0100'
 ELEVATION: 3.60'
- RSM CONTROL POINT #104211
 NAIL & DISC LS #5791 (SET)
 NORTHING: 515761.8940'
 EASTING: 1305794.3380'
 ELEVATION: 3.63'
- RSM CONTROL POINT #104215
 CAPPED IRON ROD LS #5791 (SET)
 NORTHING: 515886.3240'
 EASTING: 1305800.4890'
 ELEVATION: 4.06'

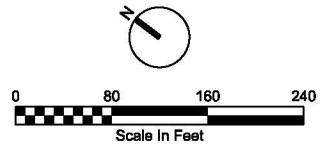


25 W CEDAR STREET, SUITE 350 PENSACOLA, FL 32502 KEVIN WADDELL PE 88025		FOR THE BROOKS BRIDGE WATER MAIN REPLACEMENT OKALOOSA ISLAND WATER SUPPLY PROJECT OKALOOSA COUNTY, FL	
ch2m: CIVIL		OVERALL SITE PLAN AND SURVEY CONTROL	
VERIFY SCALE BAR IS ONE INCH ON ORIGINAL DRAWING.			
DATE	AUGUST 2018	PROJ	691267
DWG	C-01	SHEET	of
DR		K WADDELL	
DGN		C CHILDRESS	
NO.		1	
DATE		08/17/2018	
REVISION		CHK	
BY		APVD	
RW		APVD	
BY		APVD	
J KLAUS		M STICKLEY	

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- NOTES:**
1. PIPE MUST BE FULL OF WATER DURING INSTALLATION.
 2. SEE SHEETS C-03 AND C-04 FOR LIMITS OF WORK AND CONTRACTOR RESPONSIBILITY.
 3. SEE GENERAL CONSTRUCTION NOTES ON SHEET G-02.

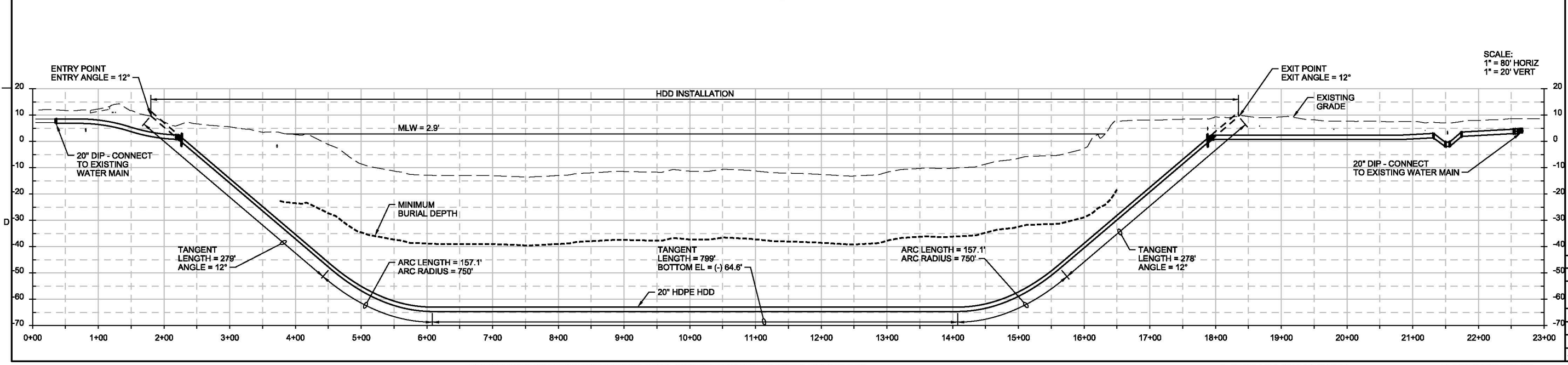


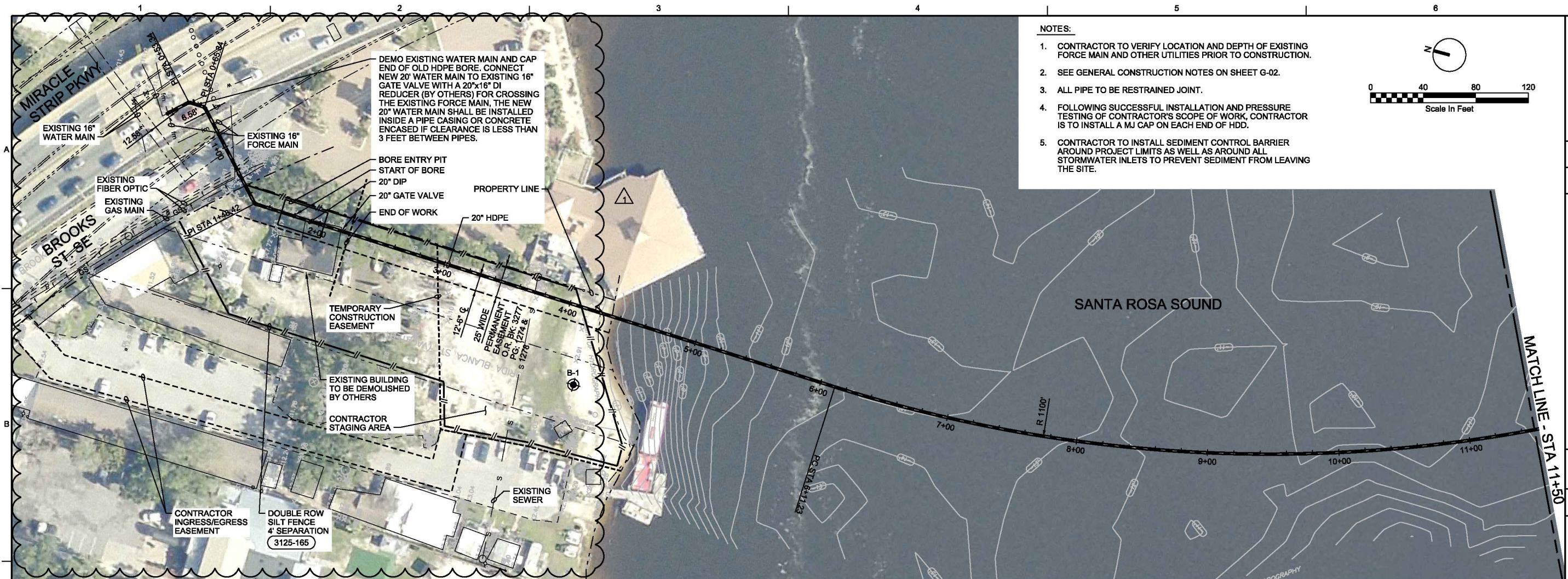
NO.	DATE	DR	CHK	REVISION
1	08/17/2018			ADDENDUM #2

25 W CEDAR STREET, SUITE 350
PENSACOLA, FL 32502
KEVIN WADDELL PE 88025

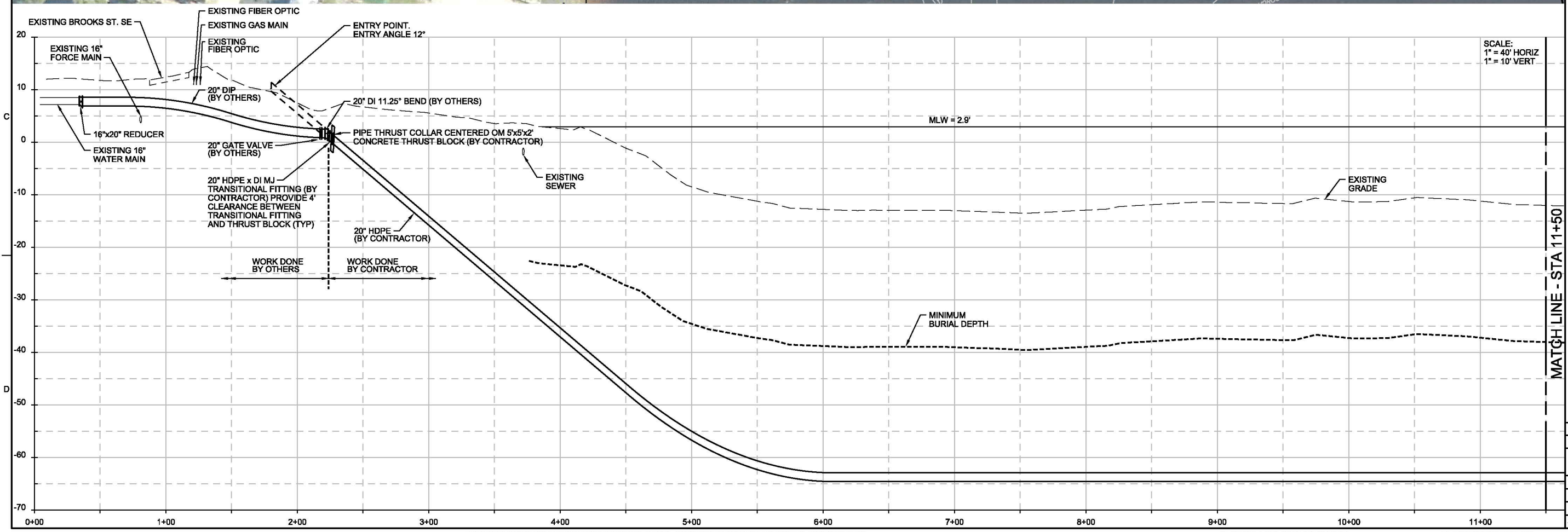
BROOKS BRIDGE WATER MAIN REPLACEMENT
FOR THE
OKALOOSA ISLAND WATER SUPPLY PROJECT
OKALOOSA COUNTY, FL

VERIFY SCALE	
BAR IS ONE INCH ON ORIGINAL DRAWING.	
DATE	AUGUST 2018
PROJ	691267
DWG	C-02
SHEET	of





- NOTES:**
1. CONTRACTOR TO VERIFY LOCATION AND DEPTH OF EXISTING FORCE MAIN AND OTHER UTILITIES PRIOR TO CONSTRUCTION.
 2. SEE GENERAL CONSTRUCTION NOTES ON SHEET G-02.
 3. ALL PIPE TO BE RESTRAINED JOINT.
 4. FOLLOWING SUCCESSFUL INSTALLATION AND PRESSURE TESTING OF CONTRACTOR'S SCOPE OF WORK, CONTRACTOR IS TO INSTALL A MJ CAP ON EACH END OF HDD.
 5. CONTRACTOR TO INSTALL SEDIMENT CONTROL BARRIER AROUND PROJECT LIMITS AS WELL AS AROUND ALL STORMWATER INLETS TO PREVENT SEDIMENT FROM LEAVING THE SITE.



25 W CEDAR STREET, SUITE 350 PENSACOLA, FL 32502 KEVIN WADDELL PE 88025		BROOKS BRIDGE WATER MAIN REPLACEMENT FOR THE OKALOOSA ISLAND WATER SUPPLY PROJECT OKALOOSA COUNTY, FL	
<p>ch2m:</p> <p>CIVIL</p> <p>WATER MAIN STA 0+00 TO 11+50 PLAN AND PROFILE</p>		<p>DATE: AUGUST 2018</p> <p>PROJ: 691267</p> <p>DWG: C-03</p> <p>SHEET: of</p>	
NO.	DATE	REVISION	CHK
1	08/17/2018	ADDENDUM #2	RW
DR	K WADDELL	APVD	M STICKLEY
DESIGN	C CHILDRESS	APVD	J KLAUS

VERIFY SCALE
BAR IS ONE INCH ON ORIGINAL DRAWING.

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BID DOCUMENTS

Mandatory Pre-Bid Meeting

PREPARED BY: Jacobs
PROJECT: Brooks Bridge WM Replacement
MEETING DATE: September 13, 2018
MEETING TIME: 10:00 AM
LOCATION: OCWS Board Conference Room
ATTENDEES: See attached Sign-In sheet

1. Attendee Sign-In and Introductions

2. Project Scope

3. Project Task Overview

- a. Contractor's Responsibilities:
 - i. A new 20" HDPE watermain across Santa Rosa Sound via HDD – fusible PVC will be accepted.
 - ii. Installation of transitional fittings and caps on pipe ends
 - iii. Pressure testing of Contractor installed pipe
 - iv. Erosion and sediment control
 - v. Traffic control for pipe fusing staging
 - vi. Site restoration to pre-construction conditions
- b. Owner's Responsibilities
 - i. Demo of existing structure on mainland side of bore
 - ii. Direct-buried pipe installation from transitional fittings to connection points
 - iii. Pressure testing of Owner installed pipe
 - iv. Disinfection and bacteriological testing of all new pipe

4. Response Requirements

- a. Provide one (1) original and two (2) copies of their ITB response
- b. Portrait orientation, unbound, and 8 ½" x 11" where practical
- c. All originals must have original signatures in blue ink
- d. Submission must comply with all requirements of the ITB
- e. Bid Opening Location:
 - i. Conference and Training Room #305
 - ii. 302 N Wilson St., Crestview, FL 32536

f. Submission Dates:

- i. **Bid Opening: September 26, 2018 at 3:00 PM CT**
- ii. **Last Day for Questions: September 17, 2018 at 3:00 PM CT**

5. Addenda

- a. Addendum #1 – Contract Dates
- b. Contact: DeRita Mason (dmason@myokaloosa.com)
- c. At least one more addendum will be issued to current plan holders, including responses to questions raised at this meeting.

6. Contract Details

- a. Contract Times
 - i. Substantial Completion – 180 days
 - 1. The project will be considered substantially complete when the HDD and transitional fittings are installed and capable of being put into service, as well as having been restored to the pre-construction site conditions. This includes successful pressure testing of the pipe.
 - ii. Final Completion – 225 days
- b. FDEP Grant Funded Project
- c. FDEP Environmental Resource Permit
 - i. Sediment and Frac-out control
- d. USACE General Permit
 - i. The Work shall comply with the National Marine Fisheries PDC's for In-Water Activities; Sea Turtle; and Standard Manatee conditions
- e. FDOT permits – OCWS has obtained permit for installation of their waterline. Contractor to obtain any additional permits that may be required.
- f. Pipe fusing staging – Drawings will be updated in an addendum to show the boundaries of the county-owned property and the property next to the fire station that is available for pipe fusing staging. This area is newly sodded and has a new irrigation system. The Contractor will be required to restore the site to pre-construction conditions.
 - i. Contractor may contact adjacent property owner for permission to use their property for pipe staging. Contact info is as follows.

Owner, Cohen Investments LLC-(Barry Cohen)
Ph. # 781-330-9527
Plat BK. 2 PG. 84A
Block 1 Lots 2 ,11 & 12
- g. Staging Area – Contractor may use the County owned property on the Island, as well as the easement on the Playground Inn property as shown on the drawings.
- h. Basis of Award – Lowest responsive, responsible bidder for total base bid price.

7. Questions and General Discussion

- a. Pipe flushing and pressure testing –
 - i. Contractor is responsible for obtaining, handling and properly disposing of water used to facilitate construction activities. Contractor to obtain any permits

that may be required. Water can be obtained from the County on Okaloosa Island, but will need to be obtained from the City of Ft. Walton Beach on the mainland side. The City's meter order form is attached to these meeting notes.

- ii. Pressure testing to be performed with water. Pneumatic air pressure testing will not be allowed.
- b. Drilling methods – Contractor may provide an alternative method to a wire line as long as a good as-builts can be provided with X,Y, and Z coordinates.

8. Site Visit

- a. A site visit was conducted with attendees immediately following the meeting.



METER ORDER FOR FIRE HYDRANT

Today's Date: _____
 Company Name: _____
 Mailing/Billing Address: _____

 Contact Person's Name: _____
 Contact Person's Phone Number: _____
 Location of hydrant (& hydrant # if known): _____
 Date Meter requested to be installed: _____
 Size meter requested (2" or 3" if available): _____
 Customer Signature: _____

OFFICE USE ONLY

Meter Number: _____
 Reading Out: _____ Date: _____ By: _____
 Reading In: _____ Date: _____ By: _____
 Actual Usage: _____

Deposit Required 401-0000-220-1100
 Account Receivable (Usage) 401-1310-343-3100
 10% Utility Tax 001-0500-314-3000
 Installation Charge 401-1310-343-3200
 Direct Pay to Reimburse

\$ 1,000.00	Date Paid _____
\$ 50.00	
	DP Date _____

Usage will be based on the In and Out Reading above, and the costs will be calculated using the following block rates:

Base Rate 0-2000 gallons	2" Mtr \$25.26 or 3" Mtr \$38.49
Block 1 2001-4000 gallons	\$3.26 per 1,000 gallons
Block 2 4001-8000 gallons	\$3.99 per 1,000 gallons
Block 3 8001 + gallons	\$5.98 per 1,000 gallons

Rates effective 10/1/17 thru 9/30/18, and until all new rates are established

Meter # and Size

Meter #1 - 3 inch
Meter #2 - 2 inch
Meter #3 - 2 inch
Meter #4 - 3 inch
Meter #5 - 2 inch

3" meter has 4" register (written 3-4)

Brooks Bridge Water Main Replacement Project

Horizontal Directional Drill Design

Brooks Bridge WM

Prepared for

Okaloosa County Water and Sewer Department

June 8, 2017
Project: 691267

Prepared by

ch2m.SM

25 W Cedar St, Suite 350
Pensacola, FL, USA 32502

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Appendices

A	HDD Drill Plan and Profile
B	BoreAid Summary Report
C	Drilling Fluid Pressure Plot
D	Analytic Solution for Allowable Borehole Pressure with Bennett and Wallin 2008 Method
E	Analytic Solution for Operational Pipe Deflection and Unconstrained Collapse

1. Introduction

Okaloosa County Water and Sewer Department (OCWS) determined that the appropriate alternative for providing a long-term, reliable source of potable water and fire protection to Okaloosa Island is to replace the existing water main with a new subaqueous pipe. The new water main will be located roughly 400 feet west of the existing main to minimize the potential for impacts to the new main in the event Brooks Bridge is replaced. The new main will be a 20-inch DR11 high-density polyethylene (HDPE) pipe installed by horizontal directional drilling (HDD) under the Sound. It will be the responsibility of the contractor to install the HDD pipe segment along with the piping at the entry and exit bore pits. OCWS will be responsible for constructing the remaining direct-buried pipe segments between the entry and exit bore pits to the connection points with the existing distribution system.

The following report outlines the crossing profile, design philosophy, stress analyses, and drill fluid pressure checks for the HDD crossing.

2. Geotechnical Data

CH2M has reviewed boring logs and geologic information provided by Larry M Jacobs Associates, Inc. to evaluate the subsurface conditions. Boring logs from the original bridge construction project were also reviewed. The soil properties provided by or derived from these data are summarized in Table 1.

In general, a fairly uniform surface layer of medium dense sand is approximately 25 feet thick under the seabed. The upper layer is underlain by a transition layer approximately 5 to 10 feet thick, comprised of loose to very loose sand, medium dense silty sand, and soft lean clay. The lower soil layer below the transition zone is very dense sand.

2.1 Assumed Soil Profile

The geotechnical data reviewed indicated the Brooks Bridge HDD crossing will launch and exit in the upper medium dense sand layer. The alignment will pass through the transition layer of silty sand, loose sand, and clay, and complete the vertical and horizontal curves within the lower very dense sand layer.

The soil properties for this evaluation were derived from the boring log data and geologic data available, the draft geotechnical data report (LMJ, 2017), and estimated using industry standards and accepted correlations.

The subsurface profile and the soil properties assumed for the HDD design are presented in Figure 1 and Table 1.

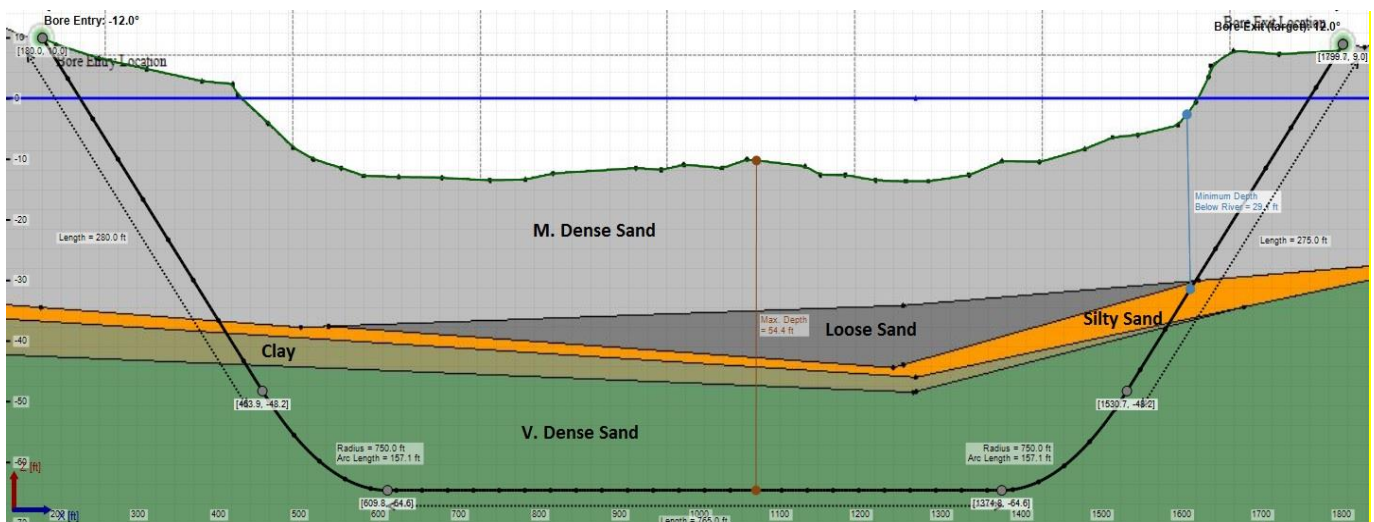


FIGURE 1

Subsurface Profile Assumed in the Brooks Bridge Water Main Crossing HDD Analysis
Distance and elevation shown in feet. See Table 1 for material descriptions and properties

TABLE 1
Soil Properties for Brooks Bridge Water Main Crossing HDD Analysis

Soil Properties	<u>Medium Dense Sand</u>	<u>Loose Sand</u>	<u>Silty Sand</u>	<u>Clay</u>	<u>Very Dense Sand</u>
Dry Unit Weight (pcf)	105	100	90	85	110
Saturated Unit Weight (pcf)	129	125	113	110	135
Friction Angle (degrees)	32	28	28	0	42
Shear Modulus (tsf)	160	35	30	12	250
Cohesion (psf)	0	0	50	250	0

2.2 Identified Geotechnical Risks

The following geotechnical risks were identified in the geotechnical assessment.

1. Reaming of the hole within the overburden. *Risk:* Past experience indicates that attempts to ream a directionally drilled borehole too rapidly can result in incomplete clearance of cuttings from the hole which, in turn, can lead to a pipeline drag section becoming stuck. Reaming in a single pass increases the risk of inadvertent fluid returns. *Mitigation:* It is expected that at least two and possibly three reaming passes will be required in order to reach the required borehole diameter.
2. Inadvertent fluid returns in overburden. *Risk:* Borehole pressures in the shallow overburden may cause inadvertent fluid returns in shallow overburden, especially as the pilot bore nears the exit point. *Mitigation:* To mitigate this risk, the pilot borehole diameter should be a minimum of 10 inches and the mud weight should be maintained under 9.2 ppg (68 lb/ft³). The mud flow rate should also be maintained under 150 gallons/minute. A frac-out contingency plan should address personnel and equipment to be on-site at all times during drilling.
3. Presence of underground utilities. *Risk:* Underground utilities are present along the crossing alignment. If steering is not controlled, the pilot bore or reaming passes may damage the existing utilities. *Mitigation:* The contractor is advised to locate and obtain clearance of these underground utilities prior to the commencement of any HDD work, and steering should be controlled within specified tolerances.

3. Horizontal Drill Profile Design

The Brooks Bridge water main HDD profile (See Appendix A) was prepared with the following design parameters:

3.1 Pipe Specifications

The following outline the design specifications of horizontal directional drill pipe.

Pipe Type:	HDPE
Pipe Specification:	DR 11 DIPS PE 4710
Average Pipe Outside Diameter:	21.6 in
Minimum Wall Thickness:	1.96 in
Design Maximum Operating Pressure:	200 psi
Mainline Test Pressure:	150 psi

The intended maximum operating pressure for the project is 65 psi, relative to the connection points to the existing main. To ensure conservative design for the HDD, DR11 rated HDPE is recommended which has a design pressure rating of 200 psi. This is greater than the project overall design pressure or 95 psi (based on the low point elevation pressure) for additional safety factor allowing flexibility in design depths and construction (actual install) tolerances. The test pressure of 150 psi is the maximum test pressures the HDD will experience during the mainline test. This is determined by the static pressure profile for the test section, and elevation difference between the critical low and HDD low point.

3.2 Drill Requirements

The crossing alignment is designed based on two primary criteria. The first criteria is that the main must stay within the OCWS 25-foot wide easement on the Fort Walton Beach side of the crossing. The second criteria is that the main must stay within the OCWS 25-foot property line bordering the Sound. OCWS will be responsible for removing an existing structure on the mainland side to provide sufficient space for drilling operations. The exit pit will be located on the island side within the OCWS property boundaries, with sufficient space for drilling operations and pipe string staging. The contractor will need to provide a traffic control plan and provide temporary access routes for access during construction. The exit point is positioned such that the bore will be able to pass underneath the existing 16-inch diameter sewer force main. Contractor should locate and expose top of pipe during drilling operations to keep adequate clearance from this force main. The bore depth on the island side needs to be followed at a minimum as to avoid dock piles present in the marina inlet.

3.3 Entry and Exit Angles

A current entry and exit angle of 12 degrees has been designed for the crossing. It should be noted that these angles are measured from horizontal, not from the existing ground surface. This exit angle may require additional breakover support.

An approximately 150 ft x 200 ft workspace will be required at the drill entrance to provide adequate space for the drilling equipment and casing requirements. For the drill exit, it is recommended that the entire pipe string be assembled prior to pullback. The pipe layout and exit area should be at least 30 ft wide and as long as the pipe string plus approximately 15 ft. The total length of the pipe string should include an additional length, which is a minimum of 4 percent of the total borepath length. This additional length mitigates the risk that the elastic rebound of the HDPE pipe pulls the pipe ends underground following pullback. The Contractor should notify the Owner/Engineer if the available space does not meet these requirements.

3.4 Design Bend Radius

The industry standard HDD minimum bend radius for HDPE pipe is 25 times the outside diameter of the pipe. Assuming a pipe diameter of 21.6 in (1.8 ft), this results in a minimum bend radius of 45 ft. However, the minimum design radius for HDPE is typically determined by the bend radius of the steel drill rods. The anticipated drill rod diameter for an HDD crossing of this size is 5 in. The industry standard minimum bend radius for steel pipe is 100 times the outside diameter of the pipe, which results in a minimum design radius of 500 ft.

The current design vertical bend radii are 750 ft for the entry and exit sides of the borepath, and the design horizontal bend radius at the center of the bore is 1,000 ft. The pilot hole should be installed at the minimum design bend radius with the following steering tolerances:

- Single-joint radius not less than 200 ft.
- Three-joint radius not less than 300 ft.
- Ten-joint radius not less than 450 ft.

4. Load and Stress Analysis

The Brooks Bridge water main has been analyzed using the method employed by the BoreAid software Version 5.0.14. The BoreAid Summary Reports are included in Appendix C. The BoreAid software calculates the pulling loads

and installation and operating stresses, as well as frac-out risk (inadvertent loss of drilling fluid to the ground surface). The pullback forces calculated with BoreAid have been checked using the ASCE/PRCI guidelines.

4.1 Pullback Buoyancy Control

A check of pipe stresses was performed and the resulting pipe stresses are within the allowable ranges, with the use of buoyancy control measures during the pullback. The design calculations contained in Appendix C utilize buoyancy control of filling the pipe full with water during pullback. If buoyancy control is not considered in the calculations, the factor of safety for unconstrained collapse during installation falls below the industry-recommended standard. Accordingly, buoyancy control measures must be used during construction. If the pipe is not filled with water during pullback, the pipe may collapse during installation.

4.2 Pulling Load Calculations

Pulling loads were analyzed using the BoreAid software. The results are found in the attached BoreAid Summary Reports in Appendix C. BoreAid calculates pulling force, stress and strain along the pipeline. The maximum pullback force with and without a factor of safety and the maximum stress developed during pullback from the BoreAid analysis are summarized in Table 2. Pullback forces applied during construction are limited to the Maximum Allowable Pullback Force shown in Table 2. Note that no buoyancy control was considered in this analysis, which is conservative for the pullback force. When maximum

TABLE 2
Maximum Pulling Force and Maximum Stress

Maximum Calculated Pullback Force ¹ (lbs)	Maximum Allowable Pullback Force ² (lbs)	Maximum Installation Bending Stress ³ (psi)	In-Service Deflection (%) ⁴
68,000	136,000	69	4.3

¹ Assumptions: Pipe assembled prior to pullback and supported on rollers. Buoyancy control is used (pipe must be filled with water during pullback), and no safety factor has been applied. Values are rounded up.

² Assumptions: Pipe assembled prior to pullback and supported on rollers. Buoyancy control is used (pipe must be filled with water during pullback), and a safety factor of 2 has been applied. Values are rounded up.

³ Tensile stress was also checked.

⁴ % = percent. Maximum allowable deflection for DR 11 HDPE pipe is 5%.

4.3 Installation Stress Analysis

Installation stresses were analyzed using the BoreAid calculations. Tensile stress, unconstrained collapse stress, and pipe deflection were checked. The results are found in the attached BoreAid Summary Reports in Appendix C. The maximum stress calculated during pullback for the crossing is shown in Table 2 above.

4.4 Operating Stress Analysis

Operating stresses including pipe deflection, unconstrained collapse, and compressive wall stress were analyzed using the BoreAid calculations. The analyses show that the pipe wall thickness is adequate for the anticipated operating stresses.

4.5 Frac-Out Analysis

Risk of inadvertent fluid returns to the surface (“frac-out”) was analyzed. No casings were assumed to be used for this analysis. Drilling fluid pressure for frac-out due to “plastic zone related to soil cover” was analyzed using the BoreAid software. BoreAid utilizes the Delft geotechnics model for this analysis, using the distance from the

borehole to the ground surface as the plastic radius in the calculation, in accordance with industry guidelines. The tabulated results are presented at the end of the BoreAid Summary Reports in Appendix C.

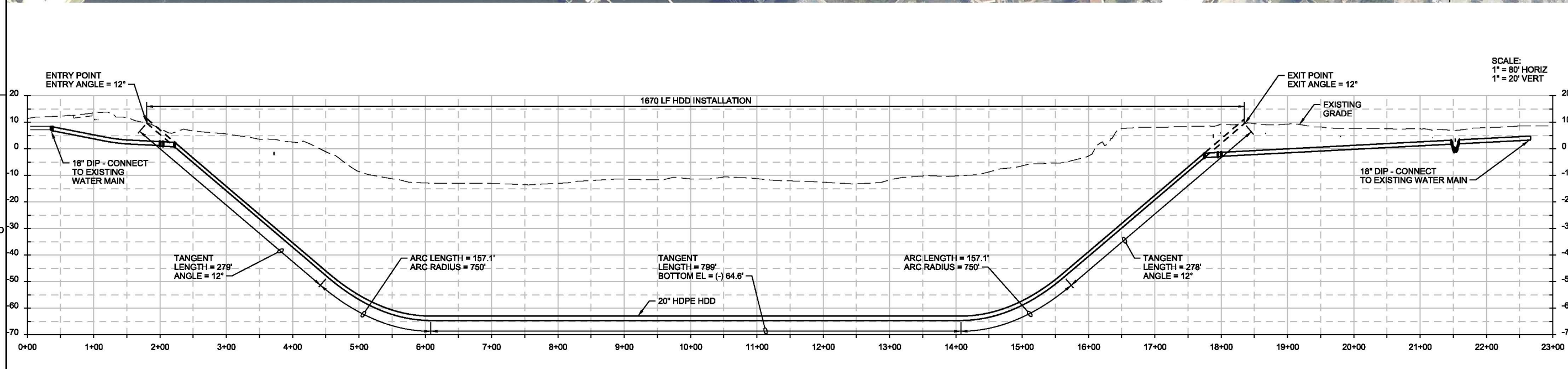
An analytic solution following the Bennett and Wallin (2008) model was performed using a factor of safety of 2.5 for the allowable drilling fluid pressure, in accordance with industry guidelines (Staheli et al, 2010). The tabulated results are presented in Appendix E.

Graphical results for the soil cover check and required borehole fluid pressure are presented in the annular pressure chart in Appendix D. Frac-out was considered for the pilot drilling operation, which is the stage of HDD construction when frac-out risk is highest.

5. Conclusions

CH2M has evaluated the anticipated configuration of the Brooks Bridge water main. The findings of our evaluation indicate the crossing can be completed in accordance with industry accepted guidelines provided the recommendations of this report are followed.

Appendix A
HDD Drill Plan and Profile



NO.		DATE	DR	REVISION	BY	APVD
K WADDELL				C CHILDRESS	J KLAUS	J KLAUS
BROOKS BRIDGE WATER MAIN OKALOOSA COUNTY, FL						
ch2m. CIVIL WATER MAIN OVERALL PLAN AND PROFILE						
VERIFY SCALE BAR IS ONE INCH ON ORIGINAL DRAWING.						
DATE		JUNE 2017				
PROJ		691267				
DWG		C-02				
SHEET		of				

60% DESIGN DOCUMENTS

REUSE OF DOCUMENTS: THIS DOCUMENT AND THE DEAS AND DESIGNS INCORPORATED HEREIN, AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF CH2M HILL AND IS NOT TO BE USED, IN WHOLE OR IN PART, FOR ANY OTHER PROJECT WITHOUT THE WRITTEN AUTHORIZATION OF CH2M HILL. © CH2M HILL 2016. ALL RIGHTS RESERVED.

Appendix B
BoreAid Summary Report



Generated Output



WARNING: The accuracy of the data obtained by the BoreAid® system is highly dependent upon accurate data gathering, data input and proper use of the software. Vermeer is not responsible for that information. BoreAid® data is not intended to replace the need for future on-site utility locating, measuring and verification procedures, which are essential for accurate placement of new underground installations and avoidance of existing utilities.

CALL YOUR ONE-CALL SYSTEM FIRST



WARNING: Always contact your local One-Call system before the start of your digging project. The BoreAid® system is intended to be used with other utility locating methods, such as the use of the One-Call system and the exposing of existing utilities by potholing.

Locate utilities before drilling. Call 811 (U.S. only) or 1-888-258-0808 (U.S. or Canada) or local utility companies or national regulating authority.

Before you start any digging project, do not forget to call the local One-Call system in your area and any utility company that does not subscribe to the One-Call system. For areas not represented by One-Call Systems International, contact the appropriate utility companies or national regulating authority to locate and mark the underground installations. If you do not call, you may have an accident or suffer injuries; cause interruption of services; damage the environment; or experience job delays.

OSHA CFR 29 1926.651 requires that the estimated location of underground utilities be determined before beginning the excavation or underground drilling operation. When the actual excavation or bore approaches an estimated utility location, the exact location of the underground installation must be determined by a safe, acceptable and dependable method. If the utility cannot be precisely located, it must be shut off by the utility company.

Input Summary

Start Coordinate	(180.00, 0.00, 10.00) ft
End Coordinate	(1800.00, 0.00, 9.00) ft
Project Length	1620.00 ft
Pipe Type	HDPE
OD Classification	DIPS
Pipe OD	21.600 in
Pipe DR	11.0
Pipe Thickness	1.96 in
Rod Length	32.00 ft
Rod Diameter	5 in
Drill Rig Location	(0.00, 0.00, 0.00) ft

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Soil Summary

Number of Layers: 5

Soil Layer #1 USCS, Sand (S), SW

From Assistant

Unit Weight: 105.0000 (dry), 129.0000 (sat) [lb/ft³]

Phi: 32.00, S.M.: 2361.11, Coh: 0.00 [psi]

Soil Layer #2 USCS, Sand (S), SW

From Assistant

Unit Weight: 100.0000 (dry), 125.0000 (sat) [lb/ft³]

Phi: 28.00, S.M.: 486.00, Coh: 0.00 [psi]

Soil Layer #3 USCS, Silt (M), ML

From Assistant

Unit Weight: 90.0000 (dry), 113.0000 (sat) [lb/ft³]

Phi: 28.00, S.M.: 416.70, Coh: 0.35 [psi]

Soil Layer #4 USCS, Clay (C), CL

From Assistant

Unit Weight: 85.0000 (dry), 110.0000 (sat) [lb/ft³]

Phi: 0.00, S.M.: 166.70, Coh: 1.74 [psi]

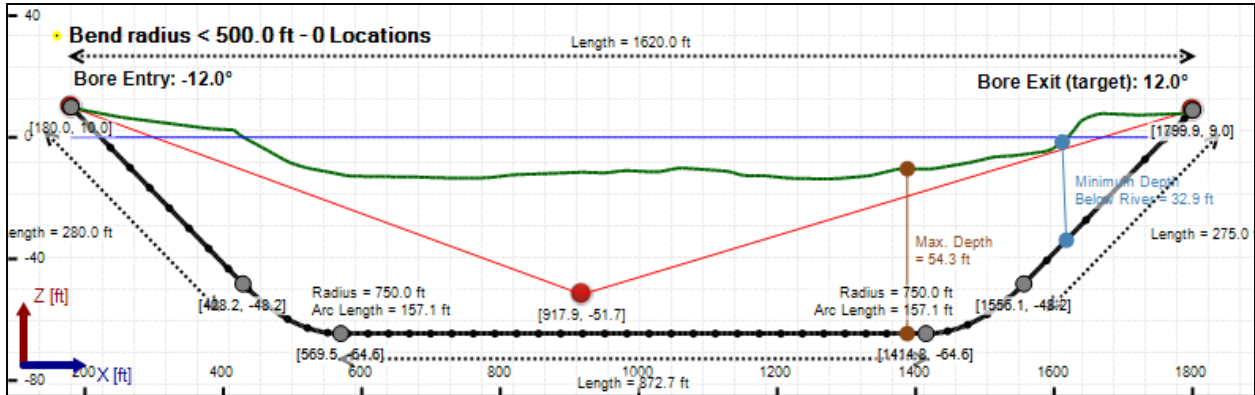
Soil Layer #5 USCS, Sand (S), SP

From Assistant

Unit Weight: 110.0000 (dry), 135.0000 (sat) [lb/ft³]

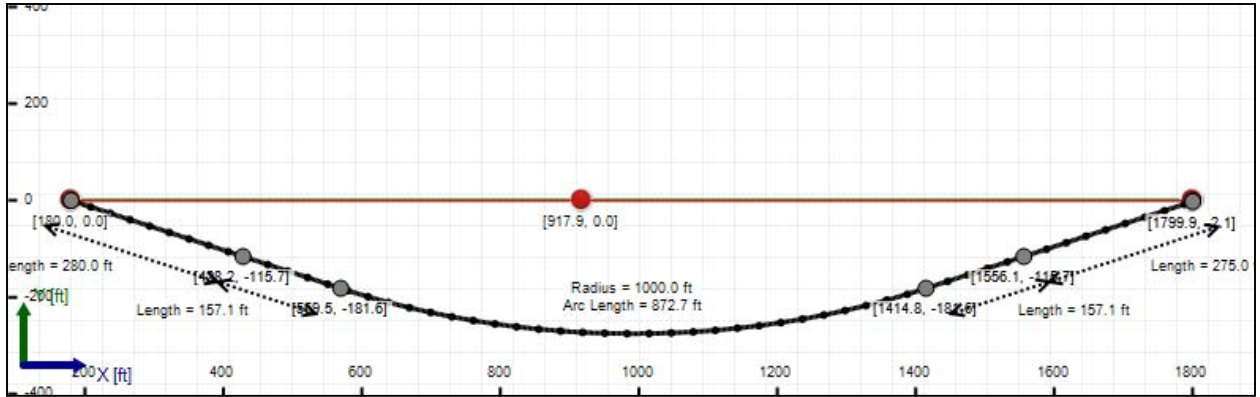
Phi: 42.00, S.M.: 3472.20, Coh: 0.00 [psi]

Bore Cross-Section View



DRAFT

Bore Plan View



Load Verifier Input Summary:

Pipe Application: Water Main
Pipe Type: HDPE
Classification: DIPS
Pipe OD: 20" (21.6")
Pipe DR: 11
Pipe Length: 1759.94 ft
Internal Pressure: 200 psi
Borehole Diameter: 2.70000012715658 ft
Silo Width: 2.70000012715658 ft
Surface Surcharge: 0 psi
Short Term Modulus: 57500 psi
Long Term Modulus: 28200 psi
Short Term Poisson Ratio: 0.35
Long Term Poisson Ratio: 0.45
Pipe Unit Weight: 59.30500 lb/ft³
Allowable Tensile Stress (Short Term): 1200 psi
Allowable Tensile Stress (Long Term): 1100 psi
Allowable Compressive Stress (Short Term): 1150 psi
Allowable Compressive Stress (Long Term): 1150 psi
Surface-pipe friction coefficient at entrance: 0.1
Surface-pipe friction coefficient in borehole: 0.3
Pipe-soil friction angle: 30
Slurry Unit Weight: 93.64118 lb/ft³
Hydrokinetic Pressure: 10 psi
Ballast Unit Weight: 62.42746 lb/ft³

In-service Load Summary:

Pressure [psi]	Deformed	Collapsed
Earth Pressure	7.0	25.1
Water Pressure	28.0	28.0
Surface Surcharge	0.0	0.0
Internal Pressure	200.0	200.0
Net Pressure	-164.9	-146.9
Deflection		
Earth Load Deflection	3.758	13.407
Bouyant Deflection	0.484	0.484
Reissner Effect	0	0
Net Deflection	4.242	13.891
Compressive Stress [psi]		
Compressive Wall Stress	-807.2	-707.7

Installation Load Summary:

Forces/Stresses	@Maximum Force	Absolute Maximum
Pullback Force [lb]	67595.9	67595.9
Pullback Stress [psi]	558.0	558.0
Pullback Strain	9.705E-3	9.705E-3
Bending Stress [psi]	0.0	69.0
Bending Strain	0	1.200E-3
Tensile Stress [psi]	558.0	616.9
Tensile Strain	9.705E-3	1.193E-2

Net External Pressure = 20.7 [psi]

Bouyant Deflection = 0.2

Hydrokinetic Force = 2290.2 lb

In-service Analysis

	Calculated	Allowable	Factor of Safety	Check
Deflection [%]	4.242	5.0	1.2	OK
Unconstrained Collapse [psi]	-198.2	67.7	-	OK
Compressive Wall Stress [psi]	-807.2	1150.0	-	OK

Installation Analysis

	Calculated	Allowable	Factor of Safety	Check
Deflection [%]	0.238	5.0	21.0	OK
Unconstrained Collapse [psi]	26.7	110.9	4.2	OK
Tensile Stress [psi]	616.9	1200.0	1.9	OK

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Maximum Allowable Bore Pressure Summary

Ream Number	Initial Diameter	Final Diameter	Estimated Maximum Pressure (Avg.)	Estimated Maximum Pressure (Local)
Pilot Bore	0.00 in	10.00 in	279.409 psi	379.856 psi
1	10.00 in	22.00 in	272.130 psi	366.402 psi
2	22.00 in	30.00 in	265.069 psi	353.667 psi
3	30.00 in	36.00 in	259.010 psi	342.970 psi

Note: The maximum bore pressures presented in this table are the maximum values along the length of the bore and not the maximum allowable at any point. The estimated maximum pressures should be compared to the estimated circulating pressures along the bore to determine potential locations of inadvertant returns.

Estimated Circulating Pressure Summary

Active	Shear Rate [rpm]	Shear Stress [Fann Degrees]
No	600	37
No	300	32
No	200	29
Yes	100	25
Yes	6	17
No	3	15

Flow Rate (Q): 120.00 US (liquid) gallon/min

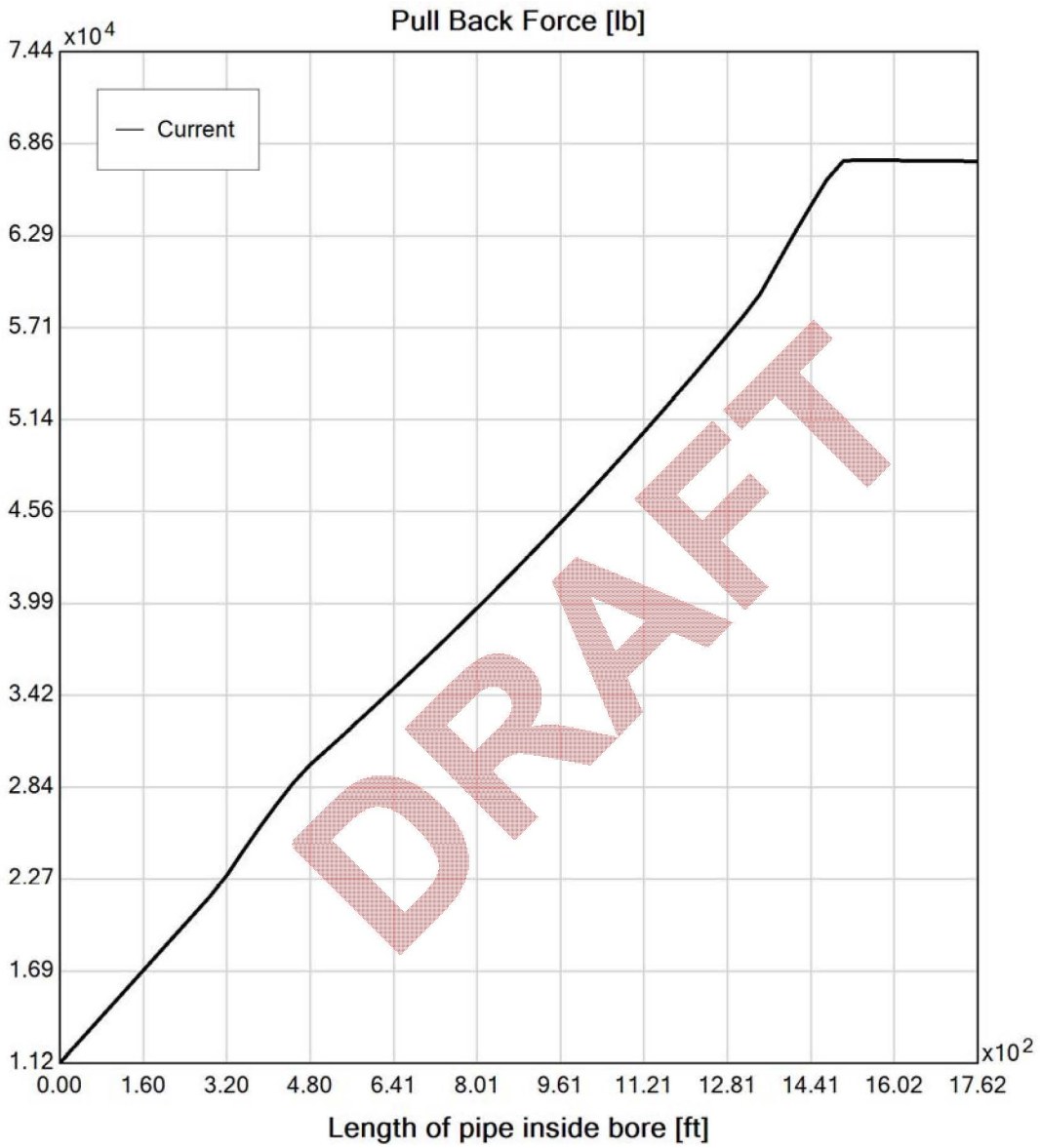
Drill Fluid Density: 68.700 lb/ft³

Rheological model: Bingham-Plastic

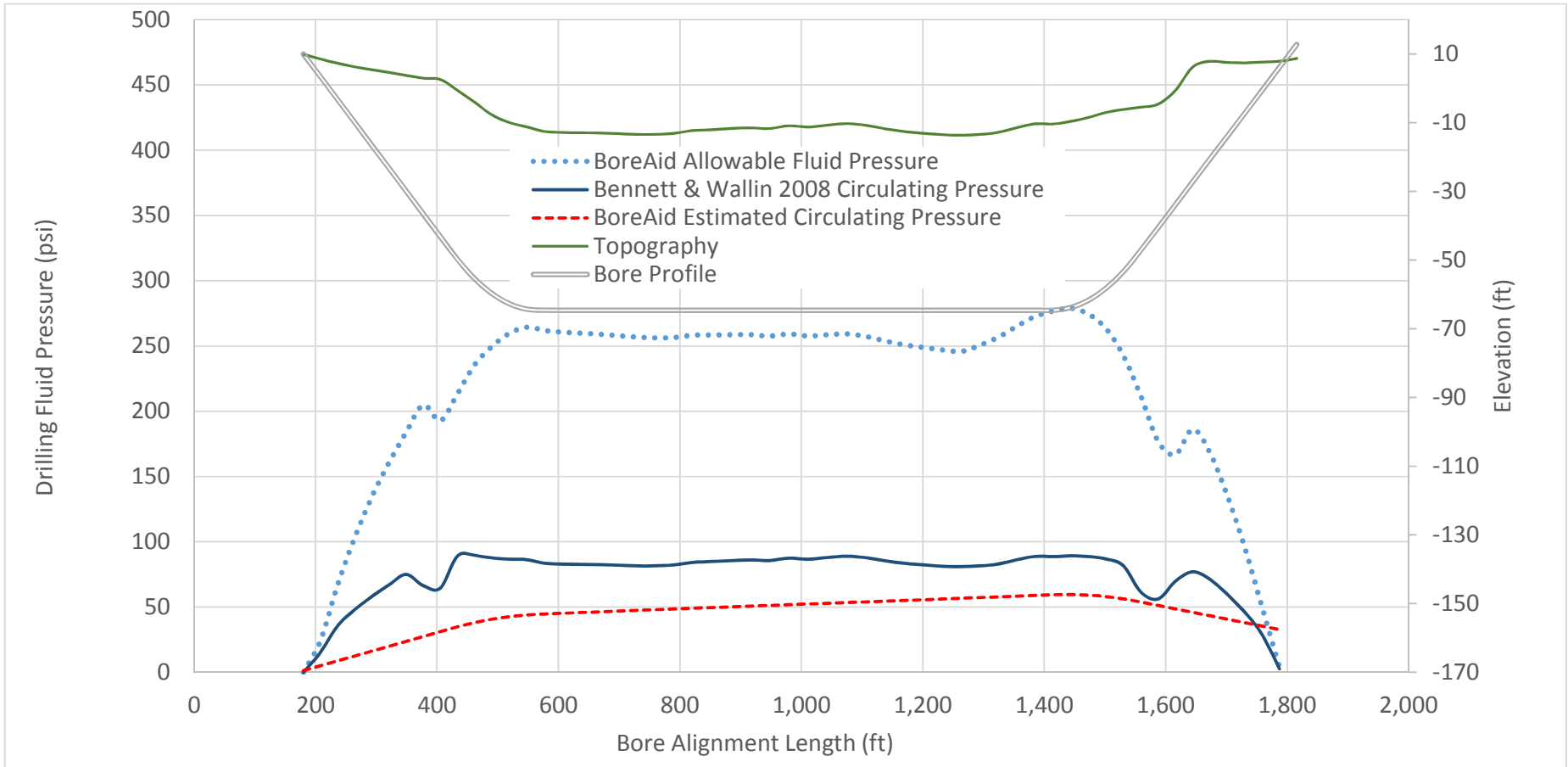
Plastic Viscosity (PV): 25.53

Yield Point (YP): 16.49

Effective Viscosity (cP): 657.0



Appendix C
Drilling Fluid Pressure Plot



Appendix D
Analytic Solution for Allowable Borehole Pressure
with Bennett and Wallin 2008 Method

1. Groundwater is assumed at el. 0m for the HDD profile.

2. Multi-layered soil profile:

Bennett 2008 states that effective stress σ' for each soil layer and sum them to find the effective stress at the point of interest.
For friction angle ϕ , cohesion c , and shear modulus G , weighted average can be used.

Soil parameters:

Soil Type	Thickness (ft)	Unit weight (pcf)	ϕ (deg)	c (psf)	G (psf)
m. dense sand	25	129	32	0.01	320000
loose sand	15	125	28	0	70000
silty sand	2	113	28	50	60000
clay	4	110	0.01	23.9184783	201434.783
v. dense sand	13	145	42	0.01	560000

Pipe info:

Pilot Bore Diameter = 10 in = 0.83333333 ft
 Pilot borehole radius R_b (ft) = 0.41666667
 Applied factor of safety (2.5 per Staheli et al 2010) = 2.5

ft (station)	BoreAid Bore Path				Estimate		Bennett Wallin 2008 Eq 1										Hydrofracture Analysis by BoreAid.																
	M/CL-ML el (ft)	Ground El. (ft)	Ground El. (ft)	Bore El. (ft)	Bore El. (ft)	Water El. (m)	Water El. (ft)	h_{tot} (ft)	h_w (ft)	σ_v (lb/ft ²)	u (lb/ft ²)	σ'_v (lb/ft ²)	$R_{p,max}$ (ft)	$\sin\phi$	$1+\sin\phi$	$c^*\cos\phi$	$c^*\cot\phi$	$(R_b/R_{p,max})^2$	$\sigma'_v \sin\phi + c^* \cos\phi / G$	$\sin\phi / (1+\sin\phi)$	P_{max} (psi)	X-Location	Y-Location	Z-Location	Length	Depth	Qmud	RhoMud	Limiting	Static	Friction	Circulating	
180.0000	10.0000	9.9107	9.9107	10.0000	10.0000	0.0000	0.0000	-0.0893	0	-11.5144	0	-11.5143852	-0.0892588	0.5299	1.52991926	0.0085	0.0160	21.7909131	0.0000	-0.34637074	-2.42646012	-0.01685042	180.0000	0.0000	10.0000	0.0000	-0.0893	100.0000	68.6700	0.0000	1.3058	0.0000	1.3058
208.2040	3.3468	8.5129	8.5129	3.3468	3.3468	0.0000	0.0000	5.16609	0	666.4256	0	666.42561	5.16609	0.5299	1.52991926	0.0085	0.0160	0.00650509	0.0011	-0.34637074	2209.7392	15.3454111	208.2040	-13.5738	3.3468	32.0000	-5.1661	100.0000	68.6700	24.4146	4.4785	0.5570	5.0355
236.4090	-3.3064	7.2920	7.2920	-3.3064	-3.3064	0.0000	0.0000	10.5983	3.30635	1367.1807	206.31624	1160.86446	10.5983	0.5299	1.52991926	0.0085	0.0160	0.00154563	0.0019	-0.34637074	5135.6298	35.6640958	236.4090	-27.1477	-3.3064	64.0000	10.5983	100.0000	68.6700	66.9974	7.6512	1.1140	8.7652
264.6130	-9.9595	6.2499	6.2499	-9.9595	-9.9595	0.0000	0.0000	16.2094	9.95952	2091.0126	621.474048	1469.53855	16.2094	0.5299	1.52991926	0.0085	0.0160	0.00066076	0.0024	-0.34637074	6902.97058	47.9372957	264.6130	-40.7215	-9.9595	96.0000	16.2094	100.0000	68.6700	103.2800	10.8239	1.6711	12.4950
292.8170	-16.6127	5.4267	5.4267	-16.6127	-16.6127	0.0000	0.0000	22.0394	16.6127	2843.0826	1036.63248	1806.45012	22.0394	0.5299	1.52991926	0.0085	0.0160	0.00035742	0.0030	-0.34637074	8373.65108	58.1503547	292.8170	-54.2954	-16.6127	128.0000	22.0394	100.0000	68.6700	134.5030	13.9967	2.2281	16.2247
321.0220	-23.2659	4.6029	4.6029	-23.2659	-23.2659	0.0000	0.0000	27.8688	23.2659	3595.0752	1451.79216	2143.28304	27.8688	0.5299	1.52991926	0.0085	0.0160	0.00022353	0.0035	-0.34637074	9641.84949	66.9572881	321.0220	-67.8692	-23.2659	160.0000	27.8688	100.0000	68.6700	160.6720	17.1694	2.7851	19.9545
349.2260	-29.9190	3.7779	3.7779	-29.9190	-29.9190	0.0000	0.0000	33.6969	29.919	4346.9001	1866.9456	2479.9545	33.6969	0.5299	1.52991926	0.0085	0.0160	0.0001529	0.0041	-0.34637074	10799.5936	74.997178	349.2260	-81.4431	-29.9190	192.0000	33.6969	100.0000	68.6700	183.7810	20.3421	3.3421	23.6842
377.4310	-36.5722	2.9592	2.9592	-36.5722	-36.5722	0.0000	0.0000	39.5314	36.5722	4867.0482	2282.10528	2584.94292	39.5314	0.5057	1.505747	2.0591	4.0715	0.00011109	0.0060	-0.33587781	9553.07036	66.3407664	377.4310	-95.0169	-36.5722	224.0000	39.5314	100.0000	68.6700	204.7690	23.5149	3.8991	27.4140
405.6350	-43.2254	2.5675	2.5675	-43.2254	-43.2254	0.0000	0.0000	45.7929	43.2254	5518.2190	2697.26496	2820.95404	45.7929	0.4655	1.46546005	21.1695	45.4808	8.2791E-05	0.0066	-0.31762043	9296.95147	64.562163	405.6350	-108.5910	-43.2254	256.0000	45.7929	100.0000	68.6700	192.7560	26.6876	4.4561	31.1437
433.8470	-49.8368	-0.6018	-0.6018	-49.8368	-49.8368	0.0000	0.0000	49.235	49.8368	6535.0750	3109.81632	3425.25868	49.235	0.5133	1.51327217	16.0063	31.1849	7.1619E-05	0.0063	-0.33918034	12839.5111	89.1632717	433.8470	-122.1680	-49.8368	288.0000	49.2350	100.0000	68.6700	213.4800	29.8404	5.0131	34.8535
462.2270	-55.4847	-4.0937	-4.0937	-55.4847	-55.4847	0.0000	0.0000	51.391	55.4847	6847.6950	3462.24528	3385.44972	51.391	0.5133	1.51327217	16.0063	31.1849	6.5736E-05	0.0063	-0.33918034	12895.0887	89.5492722	462.2270	-135.8270	-55.4847	319.9980	51.3910	100.0000	68.6700	235.7010	32.5338	5.5686	38.1024
490.7970	-59.7840	-7.7708	-7.7708	-59.7840	-59.7840	0.0000	0.0000	52.0132	59.784	6937.9140	3730.5216	3207.3924	52.0132	0.5133	1.51327217	16.0063	31.1849	6.4173E-05	0.0059	-0.33918034	12600.8118	87.5056373	490.7970	-149.5770	-59.7840	351.9950	52.0132	100.0000	68.6700	249.6910	34.5840	6.1222	40.7062
519.5080	-62.7271	-9.9835	-9.9835	-62.7271	-62.7271	0.0000	0.0000	52.7436	62.7271	7043.8220	3914.17104	3129.65096	52.7436	0.5133	1.51327217	16.0063	31.1849	6.2408E-05	0.0058	-0.33918034	12497.2761	86.7866399	519.5080	-163.3940	-62.7271	383.9930	52.7436	100.0000	68.6700	259.7090	35.9875	6.6739	42.6613
548.3050	-64.3084	-11.2454	-11.2454	-64.3084	-64.3084	0.0000	0.0000	53.063	64.3084	7090.1395	4012.84416	3077.29084	53.063	0.5133	1.51327217	16.0063	31.1849	6.1659E-05	0.0057	-0.33918034	12416.4234	86.2251623	548.3050	-177.2530	-64.3084	415.9910	53.0630	100.0000	68.6700	264.3950	36.7415	7.2236	43.9651
577.1620	-64.6046	-12.5607	-12.5607	-64.6046	-64.6046	0.0000	0.0000	52.0439	64.6046	6942.3655	4031.32704	2911.03846	52.0439	0.5133	1.51327217	16.0063	31.1849	6.4097E-05	0.0054	-0.33918034	12033.9891	83.5693687	577.1620	-191.0750	-64.6046	447.9880	52.0439	100.0000	68.6700	261.8770	36.8828	7.7714	44.6542
606.3590	-64.6046	-12.8393	-12.8393	-64.6046	-64.6046	0.0000	0.0000	51.7653	64.6046	6901.9685	4031.32704	2870.64146	51.7653	0.5133	1.51327217	16.0063	31.1849	6.4789E-05	0.0053	-0.33918034	11938.0736	82.9032886	606.3590	-204.1710	-64.6046	479.9870	51.7653	100.0000	68.6700	260.5710	36.8828	8.3188	45.2016
635.9590	-64.6046	-12.9277	-12.9277	-64.6046	-64.6046	0.0000	0.0000	51.6769	64.6046	6889.1505	4031.32704	2857.62346	51.6769	0.5133	1.51327217	16.0063	31.1849	6.5011E-05	0.0053	-0.33918034	11907.5426	82.6912677	635.9590	-216.3250	-64.6046	511.9850	51.6769	100.0000	68.6700	259.7880	36.8828	8.8662	45.7490
665.9330	-64.6047	-13.0064	-13.0064	-64.6047	-64.6047	0.0000	0.0000	51.5983	64.6047	6877.7535	4031.33328	2846.42022	51.5983	0.5133	1.51327217	16.0063	31.1849	6.5209E-05	0.0053	-0.33918034	11880.3443	82.5023906	665.9330	-227.5260	-64.6047	543.9840	51.5983	100.0000	68.6700	259.0230	36.8828	9.4136	46.2965
696.2500	-64.6047	-13.1692	-13.1692	-64.6047	-64.6047	0.0000	0.0000	51.4355	64.6047	6854.1475	4031.33328	2822.81422	51.4355	0.5133	1.51327217	16.0063	31.1849	6.5622E-05	0.0052	-0.33918034	11823.9158	82.1105265	696.2500	-237.7630	-64.6047	575.9830	51.4355	100.0000	68.6700	258.0130	36.8829	9.9610	46.8439
726.8790	-64.6047	-13.3952	-13.3952	-64.6047	-64.6047	0.0000	0.0000	51.2095	64.6047	6821.3775	4031.33328	2790.04422	51.2095	0.5133	1.51327217	16.0063	31.1849	6.6203E-05	0.0052	-0.33918034	11745.3114	81.5646222	726.8790	-247.0240	-64.6047	607.9810	51.2095	100.0000	68.6700	256.8150	36.8829	10.5084	47.3913
757.7890	-64.6047	-13.4137	-13.4137	-64.6047	-64.6047	0.0000	0.0000	51.191	64.6047	6818.6950	4031.33328	2787.36172	51.191	0.5133	1.51327217	16.0063	31.1849	6.6251E-05	0.0052	-0.33918034	11738.8629	81.5198812	757.7890	-255.3010	-64.6047	639.9800	51.1910	100.0000	68.6700	256.1960	36.8829	11.0558	47.9387
788.9470	-64.6048	-13.1358	-13.1358	-64.6048	-64.6048	0.0000	0.0000	51.469	64.6048	6859.0050	4031.33952	2827.66548	51.469	0.5133	1.51327217	16.0063	31.1849	6.5537E-05	0.0052	-0.33918034	11835.5282	82.191168	788.9470	-262.5840	-64.6048	671.9790	51.4690	100.0000	68.6700	256.4110	36.8829	11.6032	48.4861
820.3230	-64.6048	-12.3113	-12.3113	-64.6048	-64.6048	0.0000	0.0000	52.2935	64.6048	6978.5575	4031.33952	2947.21798	52.2935	0.5133	1.51327217	16.0063	31.1849	6.3487E-05	0.0055	-0.33918034	12119.5078	84.1634286	820.3230	-268.8670	-64.6048	703.9770	52.2935	100.0000	68.6700	258.1650	36.8829	12.1506	49.0336
851.8840	-64.6048	-12.0255	-12.0255	-64.6048	-64.6048	0.0000	0.0000	52.5793	64.6048	6854.1475	4031.33328	2822.81422	52.5793	0.5133	1.51327217	16.0063																	

Appendix E
Analytic Solution for Operational Pipe Deflection and
Unconstrained Collapse

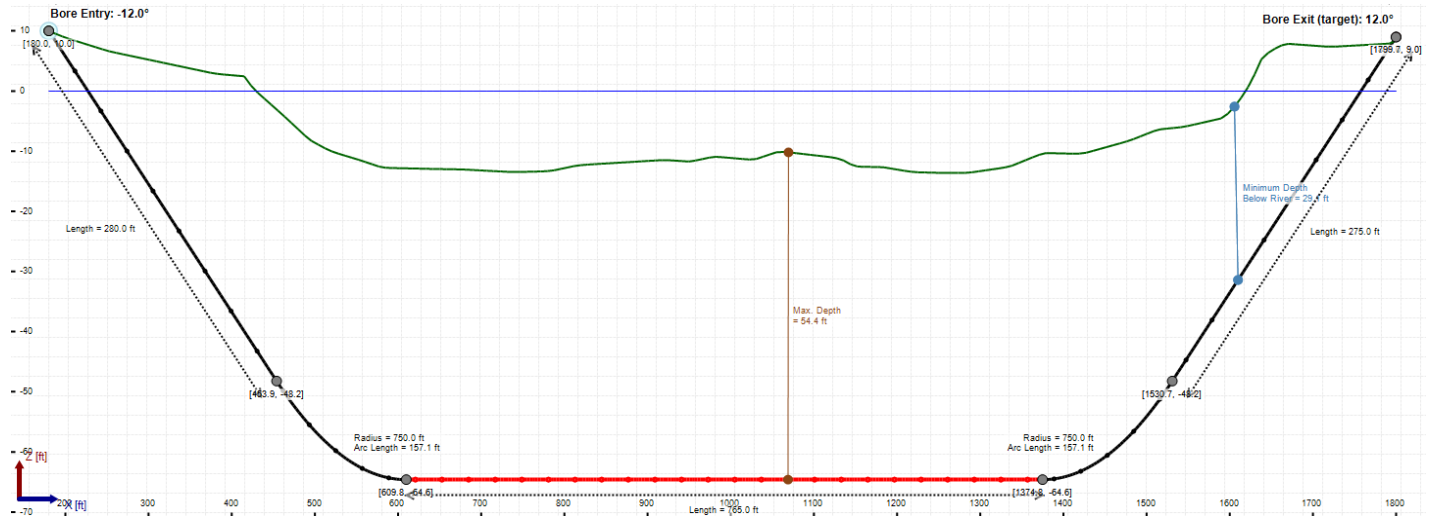
HDD ANALYSIS - PIPE DEFLECTION & UNCONSTRAINED COLLAPSE - OPERATIONAL

Brooks Bridge 20" DR11

Max Depth Location - Shutdown Occurrence - ASSUMES PIPE IS NOT EMPTIED

References:

ASTM F1962-05 Standard Guide for Use of Maxi-Horizontal Directional Drilling for Placement of Polyethylene Pipe or Conduit Under Obstacles, Including River Crossings.



Pipe Inputs

$D := 21.6\text{in} = 548.64\text{mm}$

Pipe Diameter (OD)

$DR := 11$

Dimension Ratio (OD/t)

$E := 28200\text{psi}$

Long-term Elastic Modulus for HDPE (See Table X1.1)

$\mu := 0.45$

Poisson's ratio - 0.45 (long-term) [0.35 (short term)]

$R := 750\text{ft}$

Design Bending Radius

$Y_A := 9\text{ft}$

Elevation of Pipe Connection (use lowest value of entry or exit points)

$Y_B := -64.6\text{ft}$

Elevation of Pipe at Maximum Depth

1. Earth Pressure Calculation

$B := 36\text{in} = 3\text{ft}$

"Silo" Diameter - conservative approach is to set equal to borehole diameter

$H_1 := 10\text{ft}$

$\gamma_1 := 62.4 \frac{\text{lb}}{\text{ft}^3}$

Layer 1 - Free water

$$H_2 := 23.2\text{ft}$$

$$\gamma_{2\text{sat}} := 129 \frac{\text{lbf}}{\text{ft}^3}$$

Layer 2 - M. Dense Sand

$$H_3 := 5.8\text{ft}$$

$$\gamma_{3\text{sat}} := 125 \frac{\text{lbf}}{\text{ft}^3}$$

Layer 3 - Loose Sand

$$H_4 := 4.2\text{ft}$$

$$\gamma_{4\text{sat}} := 113 \frac{\text{lbf}}{\text{ft}^3}$$

Layer 4 - Silty Sand

$$H_5 := 1.8\text{ft}$$

$$\gamma_{5\text{sat}} := 110 \frac{\text{lbf}}{\text{ft}^3}$$

Layer 5 - Clay

$$H_6 := 19.2\text{ft}$$

$$\gamma_{6\text{sat}} := 135 \frac{\text{lbf}}{\text{ft}^3}$$

Layer 6 - V. Dense Sand

$$\phi_6 := 42\text{deg}$$

Angle of Internal Friction

$$\delta_6 := \phi_6$$

Angle of Wall Friction - set equal to angle of internal friction (Eqn. X2.3)

$$K_6 := \tan\left(45\text{deg} - \frac{\phi_6}{2}\right)^2 = 0.2$$

Earth Pressure Coefficient (Eqn. X2.4)

$$H_{\text{ww}} := H_1 + H_2 + H_3 + H_4 + H_5 + H_6 = 64\text{ft}$$

Total Soil Column Above Pipe at Max Depth Point

$$\sigma_1 := \gamma_1 \cdot H_1 = 4.33\text{psi}$$

Total/Effective Stress

$$\sigma_2 := \left(\gamma_{2\text{sat}} - 9.81 \frac{\text{kN}}{\text{m}^3}\right) \cdot H_2 = 10.72\text{psi}$$

$$\sigma_3 := \left(\gamma_{3\text{sat}} - 9.81 \frac{\text{kN}}{\text{m}^3}\right) \cdot H_3 = 2.52\text{psi}$$

$$\sigma_4 := \left(\gamma_{4\text{sat}} - 9.81 \frac{\text{kN}}{\text{m}^3}\right) \cdot H_4 = 1.47\text{psi}$$

$$\sigma_5 := \left(\gamma_{5\text{sat}} - 9.81 \frac{\text{kN}}{\text{m}^3}\right) \cdot H_5 = 0.59\text{psi}$$

$$\sigma_6 := \left(\gamma_{6\text{sat}} - 9.81 \frac{\text{kN}}{\text{m}^3}\right) \cdot H_6 = 9.67\text{psi}$$

$$\kappa_6 := \frac{1 - e^{-2 \frac{K_6 \cdot H}{B} \cdot \tan\left(\frac{\delta_6}{2}\right)}}{2 \cdot \frac{K_6 \cdot H}{B} \cdot \tan\left(\frac{\delta_6}{2}\right)} = 0.3$$

Arching Factor (Eqn. X2.3)

$$P_{EV_{soil}} := (\sigma_1 + \sigma_2 + \sigma_3 + \sigma_4 + \sigma_5 + \sigma_6) = 29.3 \cdot \text{psi}$$

External Effective Earth Pressure

$$P_{EV_{arch}} := \kappa_6 \cdot P_{EV_{soil}} = 8.7 \text{ psi}$$

Arched External Earth Pressure

$$H_{static} := Y_A - Y_B = 73.6 \text{ ft}$$

Height of Static Water Column @ Shutdown

$$P_{int_static} := H_{static} \cdot 62.4 \frac{\text{lb}_f}{\text{ft}^3} = 31.89 \text{ psi}$$

Internal Static Pressure at Max Depth @ Shutdown

$$H_w := 74.6 \text{ ft}$$

Groundwater Height Above Max Depth Point

$$P_w := H_w \cdot 62.4 \frac{\text{lb}_f}{\text{ft}^3} = 32.33 \text{ psi}$$

Groundwater Pressure

$$P_{net_int} := P_{int_static} - P_w = -0.43 \text{ psi}$$

Net Internal Water Pressure in Pipe @ Shutdown
assumes: groundwater pressure is equal
around entire external circumference
+ value = internal pressure outward

$$P_{deflect} := P_{EV_{arch}} - P_{net_int} = 9.09 \text{ psi}$$

Net Pressure Acting to Deflect Pipe:
Arched Earth Load reduced by
Net Internal Water Pressure @ Shutdown

2. Earth Load Deflection

$$\Delta := \frac{0.0125 P_{deflect}}{\frac{E}{12(DR-1)^3}} = 4.8\%$$

$$\Delta_{\text{final}} := \Delta \cdot D = 26.5 \cdot \text{mm}$$

Ring Deformation (Eqn. X2.5)

Note: Table X2.1 indicates safe long-term deflection limit for DR 11 is 5.0% x D = $\Delta \times D = 26.5 \text{ mm} < 27.4 \text{ mm}$

**** OK ****



TABLE X2.1 Safe Long-Term Design Deflection values for Buried Pressurized Polyethylene Pipe

DR or SDR	Deflection Limits as % of Diameter
21	7.5
17	6.0
15.5	6.0
13.5	6.0
11	5.0
9	4.0
7.3	3.0

3. Buoyant Deflection

$$\gamma_w := 68.7 \frac{\text{lb}_f}{\text{ft}^3} = 0.04 \cdot \frac{\text{lb}_f}{\text{in}^3}$$

Weight of Drilling Fluid in Borehole - use value from BoreAid analysis

$$t_w := \frac{D}{DR} = 1.96 \cdot \text{in}$$

Minimum Wall Thickness

$$I := \frac{t^3}{12} = 0.63 \cdot \frac{\text{in}^4}{\text{in}}$$

Moment of Inertia

$$\Delta_{\text{Buoy}} := 0.1169 \cdot \gamma_w \cdot \left(\frac{D}{2}\right)^4 \cdot D = 1.95 \cdot \text{mm}$$

$$\%D_{\text{buoy}} := \frac{\Delta_{\text{Buoy}}}{D} = 0.4\%$$

Note: 0.4% < 5%

**** OK ****

4. Check Reissner Effect - additive effect of longitudinal bending
(applies at bend locations - conservative to add at max depth location)
{negligible when R > 40D and DR < 21}

$$R = 750 \text{ ft}$$

$$40 \cdot D = 72 \text{ ft}$$

$$DR = 11$$

$$z := \frac{3 \cdot (1 - \mu^2) \cdot (D - t)^4}{16 \cdot t^2 \cdot R^2} = 0.00004$$

Intermediate Factor

$$\Delta_R := \left(\frac{2}{3}\right) \cdot z + \left(\frac{71}{135}\right) \cdot z^2 = 0.0024\%$$

Reissner Ovality

$$\Delta + \Delta_R = 4.8\%$$

Max Ovality Deflection

5. Unconstrained Collapse

$FS := 2$

Safety Factor for Unconstrained Collapse (recommended = 2.0)

$f_o := .62$

Ovality Compensation Factor (See Fig. 2) $\Delta = 4.83\%$

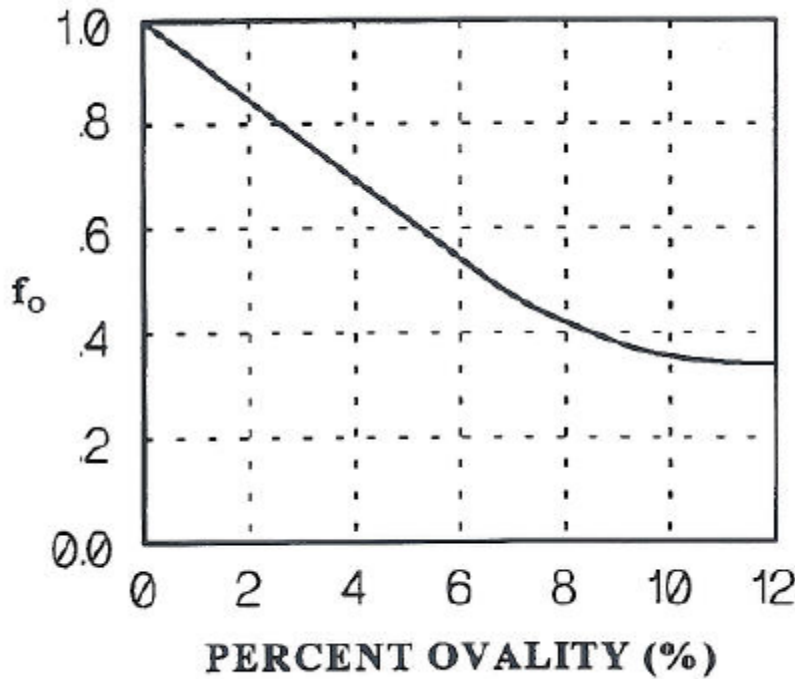


FIG. 2 Ovality Compensation Factor

$$P_{ua} := \frac{2 \cdot E}{(1 - \mu^2)} \cdot \left(\frac{1}{DR - 1} \right)^3 \cdot \frac{f_o}{FS} = 21.9 \text{ psi}$$

Allowable External Collapse Pressure (Eqn. 5)

$$P_{tot_ext} := P_{EV_arch} + P_w = 41 \text{ psi}$$

Total External Pressure on Pipe (8.2.3: effective earth pressure [reduced for arching] + hydrostatic pressure)

$$P_{int_static} = 31.89 \text{ psi}$$

Internal Pressure on Pipe @ Shutdown Case

$$P_{net} := P_{tot_ext} - P_{int_static} = 9.1 \text{ psi}$$

Net External Pressure on Pipe @ Shutdown Case (assumes pipe is full)

Check P_{ua} with the value from Table X3.1:

$$P_{crit} := 71 \text{ psi}$$

Critical Buckling Pressure (Table X3.1) - 50 yrs for Long Term - 138psi

TABLE X3.1 Critical Collapse Pressure for Unconstrained HDPE Pipe^{A,B,C} at 73°F

NOTE—Table does not include ovality compensation or safety factor.

Service Life	Pipe SDR, psi, ft H ₂ O, in Hg						
	7.3	9	11	13.5	15.5	17	21
Short-term	1003, 2316, 2045	490, 1131, 999	251, 579, 512	128, 297, 262	82, 190, 168	61, 141, 125	31, 72, 64
100 h	488, 1126, 995	238, 550, 486	122, 282, 249	62, 144, 127	40, 92, 82	30, 69, 61	15, 35, 31
50 years	283, 653, 577	138, 319, 282	71, 163, 144	36, 84, 74	23, 54, 47	17, 40, 35	9, 20, 18

^AAxial Tension during pull-back reduces collapse strength.

^BFull vacuum is 14.7 psi, 34 ft water, 30 in Hg.

^CMultipliers for temperature rerating:

$\frac{60^{\circ}\text{F}(16^{\circ}\text{C})}{1.08}$	$\frac{73.4^{\circ}\text{F}(23^{\circ}\text{C})}{1.00}$	$\frac{100^{\circ}\text{F}(38^{\circ}\text{C})}{0.78}$	$\frac{120^{\circ}\text{F}(49^{\circ}\text{C})}{0.63}$
---	---	--	--

$$P_{allow} := P_{crit} \left(\frac{f_o}{FS} \right) = 22 \text{ psi}$$

Allowable Collapse Pressure - should approx. equal P_{ua} from Eqn. 5

$$P_{ua} = 21.9 \text{ psi}$$

P_{ua} exceeds P_{net} (see 8.2.4.2)

**** OK ****

$$P_{ua} = 21.9 \text{ psi}$$

$$P_{net} = 9.1 \text{ psi}$$

PRE-BID CONFERENCE

ITB: WS 66-18 Brooks Bridge Water Main Replacement

DATE/TIME: September 13, 2018/ 10:00 AM PURCHASING REPRESENTATIVE: DeRita Mason

PLEASE PRINT NEATLY & CLEARLY! IF AVAILABLE, PLEASE LEAVE BUSINESS CARD

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Jacobs	Kevin Waddell	ph: 850-941-7279	Kevin.waddell@jacobs.com

* = added up not attending meeting

